



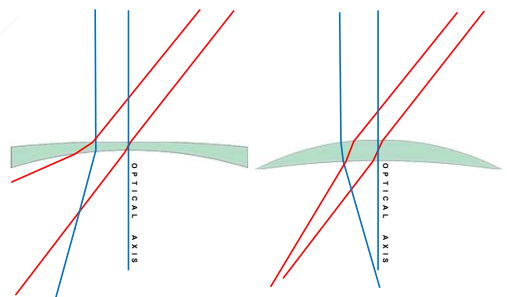
Compensated Powers (and other ophthalmic conundrums)


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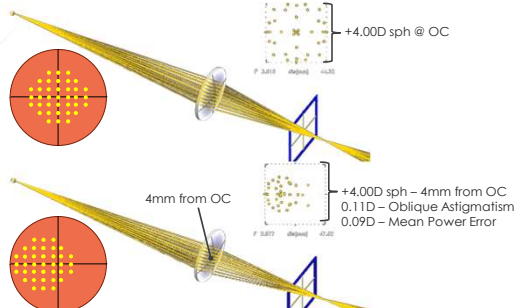


What are Compensated Powers?





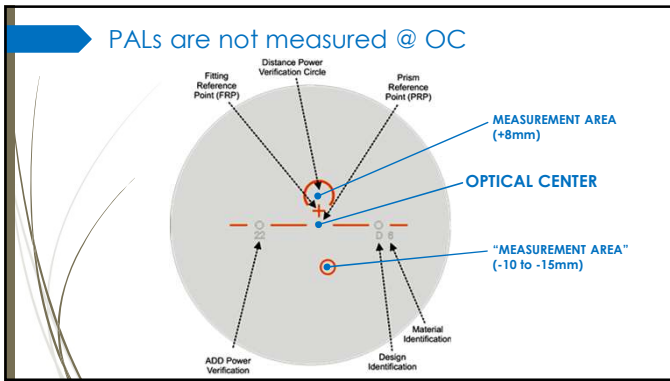
Same Lens- Different Results

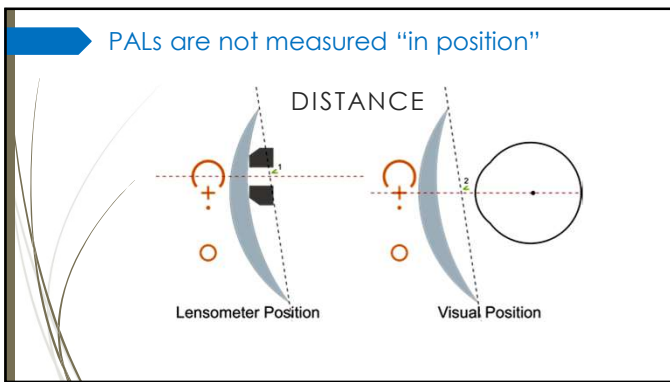


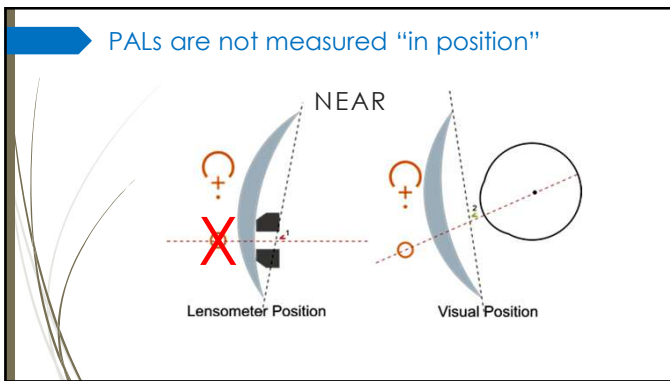
+4.00D sph @ OC

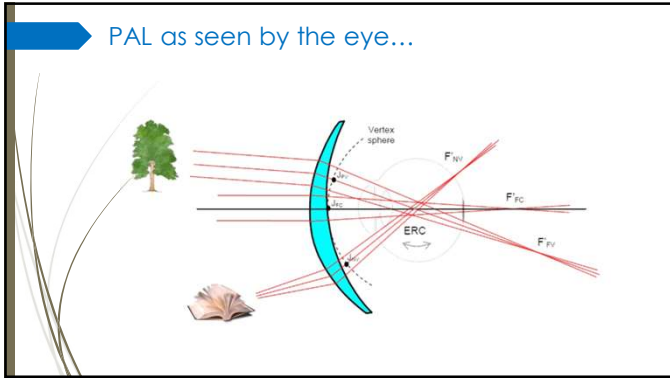
4mm from OC

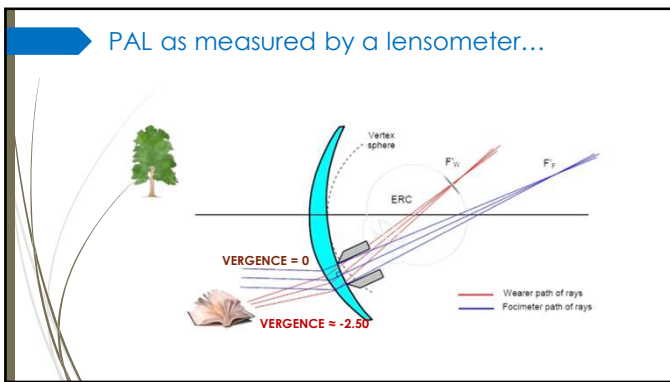
+4.00D sph - 4mm from OC
0.11D - Oblique Astigmatism
0.09D - Mean Power Error

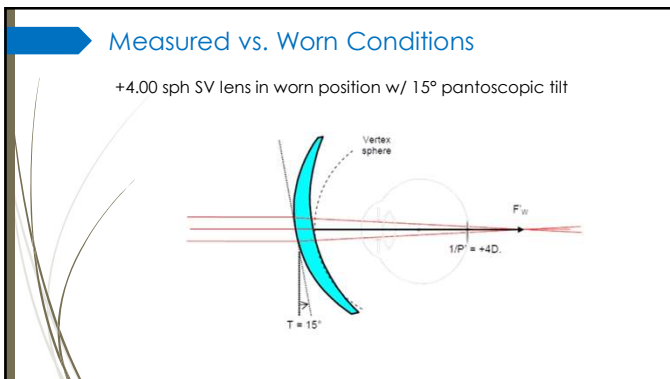












Measured vs. Worn Conditions

+4.00 sph SV lens in worn position w/ 15° pantoscopic tilt
 Lens is not measured in worn position...

Measured vs. Worn Conditions

+4.00 sph SV lens in worn position w/ 15° pantoscopic tilt
 Lens is tilted 15° away from worn position...

Measured vs. Worn Conditions

ANGLE (°)	SPHERE (D.)	CYLINDER (D.)	AXIS (°)
0	4.00	0.00	-
3	3.99	0.01	90
6	3.94	0.04	90
9	3.87	0.10	90
12	3.77	0.17	90
15	3.64	0.27	90

Measured focimeter powers of an as-worn +4D. SV calculated lens taking into account a tilt of ANGLE.

Has the power really been "compensated" (changed)?
 No. The lens is still a +4.00 sph.
 "Compensated" power indicates how the lensometer will see the lens.

Methods of Measurement

All lensmeters are not created equal...

Methods of Measurement

+5.00 -4.00 x 090 FOA vs IOA (CV)

	Min. sphere (D.)	Max. sphere (D.)
FOA	1.03	5.06
IOA	0.99	4.98
Discrepancies (FOA - IOA)	+0.04	+0.08

ADD measurement discrepancy FOA (CV v CX)

	Convex	Concave
Mean sphere (D.)	3.05	2.92
Far vision	5.72	5.40
Near vision	2.48	2.67
Discrepancies (Concave - Convex)		+0.19

ADD measurement discrepancy IOA (CX v Wearer)

	Convex	Wearer
Mean sphere (D.)	2.95	3.05
Far vision	5.46	5.90
Near vision	2.51	2.84
Discrepancies (Wearer - Convex)		+0.33

Measured power ≠ ordered power

Wearer prescription →

Expected focimeter measurements →

G/L	DD	Sph	Cyl	Axe	Add
727 100	70/75	+3.25	+0.75	090	+1.25
		+3.12	+0.62	025	+1.14

If you simply *must* verify near power...

- Use FRONT vertex power for Traditional & Dual-Sided PALs
 - mount lenses "backwards" on lensometer
 - measure distance power through distance verification circle
 - measure power through near verification circle
 - calculate the difference and compare to *compensated* value

(For FBS PALs, measure BACK vertex power)

First Reading **Second Reading**

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Lens Geometry Also Has an Impact

- Surface Geometry**
 - Curvature
 - P-value (asphericity)
 - Thickness
- Positional Geometry**
 - Pantoscopic Angle (vertical tilt)
 - Wrap Angle (horizontal tilt)
 - Vertex Distance
 - Optical Center Position

Geometric Impact on Measurement

Face Form Parameters:

- Pantoscopic: 6.0
- Facial Wrap: 7.0
- Eyelets A: 12.0 mm
- Depth B: 42.0 mm
- Bridge DBL: 12.0 mm

Base Curve: 5.00

Sphere Power	Cylinder Power	Cylinder Axis	Add Power	Interpup Distance	Pupil Above	Base Curve	Center Thickness	Vertex Distance
00	+4.00	180	+2.00	52.0	5.0	5.00	12.0	Relaxed
05	+4.00	180	+2.00	52.0	5.0	5.00	12.0	Fitted

Compensated Prescription Data:

Near Sphere	Near Cylinder	Near Axis	Near Pupil Distance	Reading Below OC	Prime at Reading	Vertical Mag	Horizontal Mag	Minimum Blank Size
00	+3.95	18.15	130	29.8 mm	12.4 mm	14.97 EU	+8.7%	+8.7%
05	+3.79	18.15	132	30.2 mm	13.1 mm	14.03 EU	+5.4%	+5.4%

Compensated Powers

“Compensation” does NOT change the ordered power...
...compensation indicates how the ordered power will be seen by the lensometer!

What is Chromatic Aberration?

Lateral Chromatic Aberration (LCA)

Axial Chromatic Aberration (ACA)

What is Chromatic Aberration?

AXIAL CHROMATIC ABERRATION

ACA = $\frac{\text{POWER}}{\text{ABBE}}$

LATERAL CHROMATIC ABERRATION

LCA = $\frac{\text{PRISM}}{\text{ABBE}}$

Abbe Value and Chromatic Aberration

Abbe Facts (Fabbies ☺)


- Plano lenses produce ZERO chromatic aberration
- No LCA at the optical center- regardless of power (if blur occurs looking straight ahead, its not LCA)
- Human eye has >1.00 diopter of ACA
- Studies show >0.12D CA may be noticeable to some (>3.75D of power/prism is required for 0.12D CA)
- If patient non-adapts to poly, but accepts 1.67... the problem was NOT chromatic aberration
- AR does NOTHING to reduce chromatic aberration

Abbe Value and Chromatic Aberration

Abbe Facts (Fabbies ☺)

- Plano lenses produce ZERO chromatic aberration

$$0 \text{ ACA} = \frac{0 \text{ POWER}}{\text{ABBE (ANY VALUE)}}$$


$$0 \text{ LCA} = \frac{0 \text{ PRISM}}{\text{ABBE (ANY VALUE)}}$$


Abbe Value and Chromatic Aberration

Abbe Facts (Fabbies ☺)

- No LCA at the optical center- regardless of power

If the patient has blur in the center of the lens, the problem is not chroma (unless the lenses are exceptionally high power).

$$0 \text{ LCA} = \frac{0 \text{ PRISM}}{\text{ABBE (ANY VALUE)}}$$


Abbe Value and Chromatic Aberration

Abbe Facts (Fabbies ☺)

- If patient non-adapts to poly, but accepts 1.67... the problem was NOT chromatic aberration

$$\text{LCA} = \frac{0.161 \text{ PRISM}}{31 \text{ ABBE (Poly)}}$$

$$\text{LCA} = \frac{0.156 \text{ PRISM}}{32 \text{ ABBE (1.67)}}$$

Abbe Value and Chromatic Aberration

Abbe Facts (Fabbies ☺)

- Studies show >0.12D CA may be noticeable to some

7.5 mm
(15° eye rotation)

-5.00 sph (BC 2.75) and/or
+5.00 sph (BC 8.25)

$$\text{LCA} = \frac{3.75 \text{ PRISM}}{\text{ABBE}}$$

Chromatic Aberration is NOT an issue in ANY material (for 93.7% of wearers at least)!

Abbe Value and Chromatic Aberration

Abbe Facts (Fabbies ☺)

- Studies show >0.12D CA may be noticeable to some

CR-39 (58) = 0.06Δ LCA = 20/21
 Trivex (44) = 0.09Δ LCA = 20/22
 Polycarb (30) = 0.13Δ LCA = 20/23
 1.60 MR-8 (41) = 0.09Δ LCA = 20/22
 1.67 MR-7 (32) = 0.12Δ LCA = 20/23

$$\text{LCA} = \frac{3.75 \text{ PRISM}}{\text{ABBE}}$$


LATERAL CA	VISUAL ACUITY
0.05 Δ	20/21
0.10 Δ	20/22
0.15 Δ	20/24
0.20 Δ	20/26
0.25 Δ	20/28
0.30 Δ	20/31
0.35 Δ	20/34
0.40 Δ	20/39
0.45 Δ	20/44
0.50 Δ	20/51
0.55 Δ	20/60
0.60 Δ	20/75

Chromatic Aberration is NOT an issue in ANY material (for 93.7% of wearers at least)!

Effect of Chromatic Dispersion of a Lens on Visual Acuity. Meiss, D. & Obrecht, G. Am. J. of Optom. & Physiol. Optic. 65:25-26, 1988.

How No-Glare Works

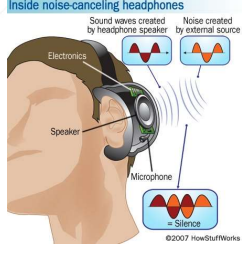
Eliminating Reflections with Reflections
 Light waves can be "cancelled" through a process called "destructive interference..."



...light waves in opposition cancel each other out

How No-Glare Works

Inside noise-canceling headphones

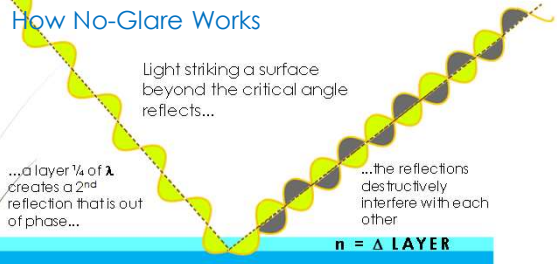


Sound waves created by headphone speaker
 Noise created by external source
 = Silence

Noise cancellation headphones use the same principle...

How No-Glare Works

Light striking a surface beyond the critical angle reflects...

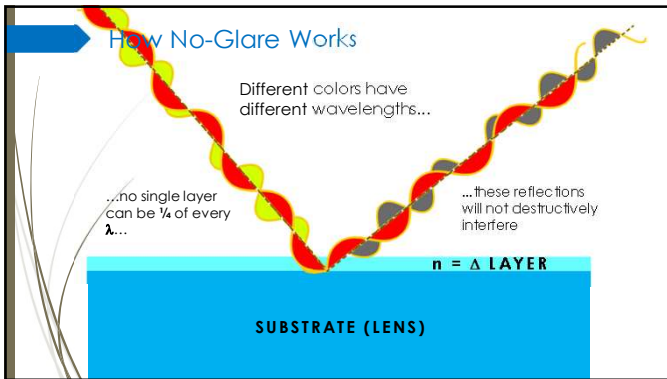


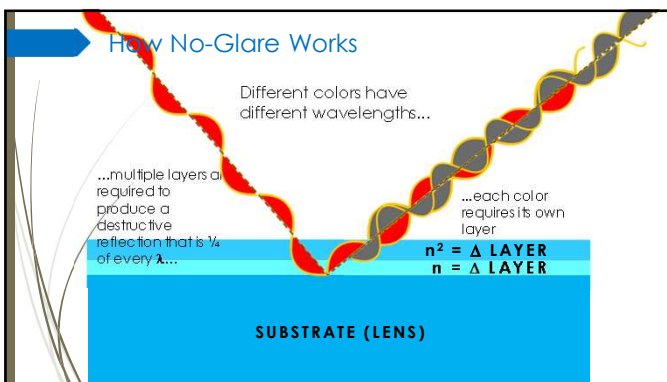
...a layer $\frac{1}{4}$ of λ creates a 2nd reflection that is out of phase...

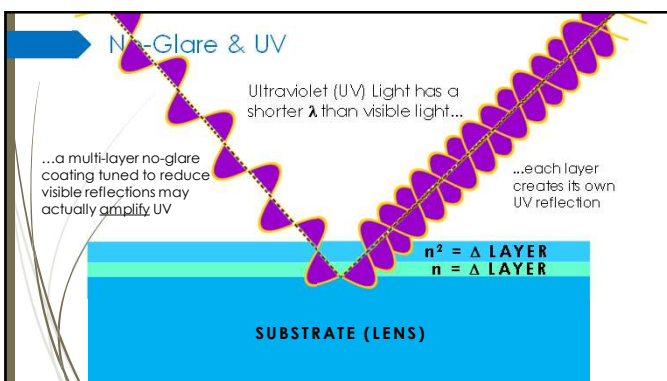
...the reflections destructively interfere with each other

$n = \Delta$ LAYER

SUBSTRATE (LENS)








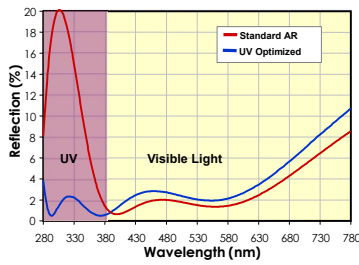
No-Glare & UV

Inside noise-canceling headphones



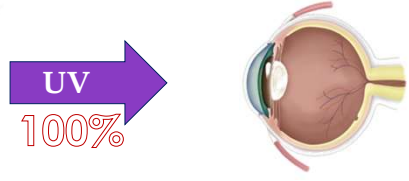
Imagine the result if the cancellation sound in the headphone was the SAME (in phase) as the external noise ...

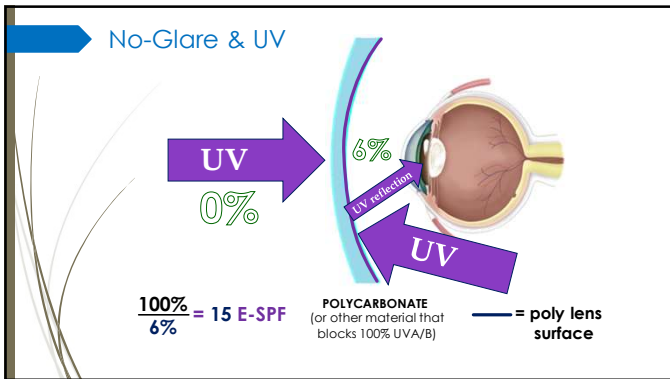
No-Glare & UV

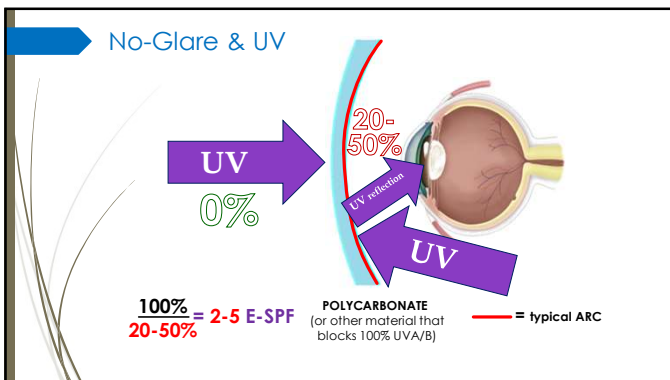


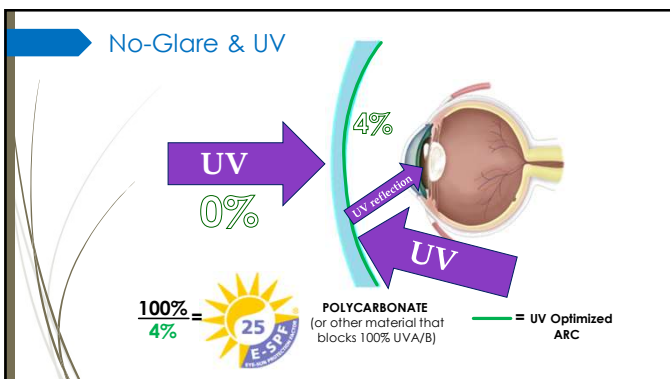
Imagine the result if a no-glare coating created UV reflections IN PHASE with each other...

No-Glare & UV









What is ANSI?

AMERICAN NATIONAL STANDARD

ANSI Z80.1-2010

1.2 Purpose

This standard reflects the shift in utilization from mass-produced lenses to a basic dependence upon custom-processed lenses at the laboratory level. It does not represent tolerances that describe the state-of-the-art of the ophthalmic laboratory, but provides quality goals for new, pristine lenses prepared to individual prescription. The individual performance parameters listed in this standard can be achieved reliably. However, it is difficult to meet all of the requirements simultaneously in any given lens or mounted pair. The fact that, under rigorous application of this standard, a significant number of spectacles (approximately 25%, based upon industry data) will not achieve all parameters simultaneously, must be accepted as a reflection of the state-of-the-art. As such, this standard expresses desirable technical concepts that provide a frame of reference for safety and effectiveness and is not designed as a regulatory instrument.

...and what ISN'T it?

5.1 General

Both uncut and edged finished lenses shall meet the following requirements. For lenses produced with compensations to account for as worn correction, the tolerances in the tables in clause 5 apply to those values specified by the manufacturer and not to the prescribed RX.

5.1.1 Distance Refractive Power (Back Vertex Power)

5.1.1.1 Single Vision and Multifocal Lenses

Table 1 – Tolerance on Distance Refractive Power (Single-Vision and Multifocal Lenses)

Sphere Meridian Power	Tolerance on Sphere Meridian Power	Cylinder ≥ 0.00 D ≤ -2.00 D	Cylinder > -2.00 D ≤ -4.50 D	Cylinder > -4.50 D
From -6.50 D to +6.50 D	± 0.13 D	± 0.13 D	± 0.15 D	$\pm 4\%$
Stronger than ± 6.50 D	$\pm 2\%$	± 0.13 D	± 0.15 D	$\pm 4\%$

5.1.1.2 Progressive Addition Lenses

Table 2 – Tolerance on Distance Refractive Power (Progressive Addition Lenses)

Sphere Meridian Power	Tolerance on Sphere Meridian Power	Cylinder ≥ 0.00 D ≤ -2.00 D	Cylinder > -2.00 D ≤ -3.50 D	Cylinder > -3.50 D
From -8.00 D to +8.00 D	± 0.16 D	± 0.16 D	± 0.18 D	$\pm 5\%$
Stronger than ± 8.00 D	$\pm 2\%$	± 0.16 D	± 0.18 D	$\pm 5\%$
